

AD-A168 014

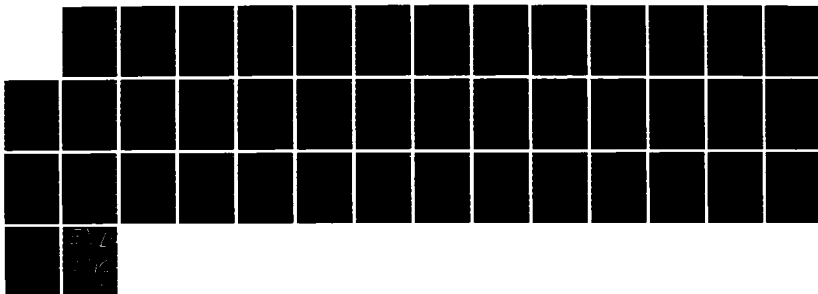
CRACK-TIP FIELDS IN A VISCOPLASTIC MATERIAL(U)
NORTHWESTERN UNIV EVANSTON IL STRUCTURAL MECHANICS LAB
J D ACHENBACH ET AL. APR 86 NU-SNL-TR-86-1
N00014-76-C-0063

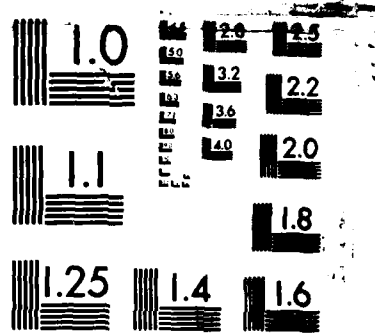
1/1

UNCLASSIFIED

F/G 28/11

NL





MICROCOPY RESOLUTION TEST CHART
NATIONAL BUREAU OF STANDARDS-1963-A

AD-A168 014

CRACK-TIP FIELDS IN A VISCOPLASTIC MATERIAL

J. D. Achenbach, N. Nishimura and J. C. Sung

Department of Civil Engineering
Northwestern University
Evanston, IL. 60201

Office of Naval Research

N00014-76-C-0063

April 1986

NU-SML-TR-86-1

Approved for public release; distribution unlimited

86 5 20 084

DTIC FILE COPY

Abstract

An integral representation for the particle velocity in terms of a Green's function and certain linear combinations of the inelastic strain rates has been used in this paper, both for a numerical method to compute full field solutions and to develop unequivocal asymptotic expressions for the near-tip fields. Specific results have been obtained for a stationary crack in a solid whose constitutive behavior is represented by the Bodner-Partom model. It is shown that the leading term of the near-tip particle velocity is of order $r^{1/2}$, and the higher-order terms are of the forms $r \log r$ and r . Expressions have been derived for the angular variations and for the multiplying time-dependent intensity factors. The $r \log r$ term is absent for the Mode-II case. Two questions have been addressed in further detail: the dependence of the multiplying terms on time and the importance of the higher-order terms. The numerical results show a stress intensity factor which decays with time. At a small distance from the crack tip the numerically computed normalized opening stress $\tau_{22}(x_1, 0, t)/\tau_{22}(x_1, 0, 0)$ has been compared with a one-term asymptotic representation, i.e., with $K_I(t)/K_I(0)$. The two curves diverge at very small values of time. The inclusion of a second term in the asymptotic expression for the stress gives very acceptable agreement as time increases.



Handwritten marks and stamps in the bottom right corner, including a large "A" and a vertical stamp with the number "11".

1. Introduction

A clear understanding of the mathematical structure of the fields of stress and deformation near a stationary crack tip is an essential prerequisite to an investigation of conditions for the onset of crack propagation. In a visco-plastic solid the fields in the immediate vicinity of a crack tip can be very intricate. In this paper near-tip visco-plastic fields have been investigated in detail for a class of constitutive models for which the inelastic strain rate approaches a bounded value as the stresses increase beyond bounds. The Bodner-Partom model [1], which has been shown to describe the mechanical response of a wide class of materials, displays this particular behavior of the inelastic strain rate.

Fields near a crack tip are usually analyzed asymptotically by assuming a near-tip field of the general form $r^p f(\theta)$. When this expression is substituted into the governing equations and into appropriate boundary conditions, and terms of equal order in r are collected, there results a nonlinear eigenvalue problem, which yields both p and $f(\theta)$. For visco-elastic solids this method was used by Riedel [2] and Riedel and Rice [3], who investigated the near tip fields of stationary cracks for Mode III and Mode I, respectively. They considered a viscoelastic constitutive equation of the power law type. For the Mode I case their asymptotic solution displays the well-known HRR singularity if the power is greater than one. When the power is less than one, the solution becomes square-root singular.

Hui & Riedel [4] considered quasistatically moving cracks for both Mode I and Mode III conditions. When the power is greater than 3, their singularity is different from both the HRR and the square-root singular forms, while for a power less than 3 it reduces to a square-root singularity. Lo [5] followed the Hui-Riedel approach, but he took into account the effect of inertia.

The implications of square-root singular as crack-tip fields for viscoplastic solids have been explored by Hart [6] and Freund and Hutchinson [7]. For a Mode III quasi-static steady-state analysis, Hart [6] related the stress intensity factor at the tip to the corresponding far-field quantity. He also discussed transient cases on the basis of certain assumptions. Freund and Hutchinson [7] developed a similar relation between the tip and the far-field stress intensity factors for the dynamic steady-state Mode I case, using an essentially linear relation between the stress and the inelastic strain rate.

In this paper a more fundamental approach towards the computation of near-tip fields is presented, in the sense that asymptotic forms are not assumed a-priori. Instead, the particle velocity field is expressed by a representation integral over the complete domain of the cracked body. This integral involves an elastic Green's function and linear combinations of the inelastic strain rates. Since the inelastic strain rates are bounded at the crack tip, the integral can be expanded in terms of the distance to the crack tip, to yield an unequivocal expression for the near-tip field. Details have been worked out for a stationary crack tip. It is shown that the leading term of the particle velocity is of order $r^{\frac{1}{2}}$, and the next terms are of the forms $r \log r$

and r . Expressions have been derived for the angular variations and for the multiplying time-dependent intensity factors. The $r \log r$ term is absent for the Mode-III case. Two points are of interest: the dependence of the multiplying terms on time and the importance of the higher-order terms.

The representation of the particle velocity in terms of an appropriate Green's function and the time-rates-of-change of the inelastic strains has not only been used to obtain near-tip asymptotic expansions of relevant field variables, but also to develop numerical solutions by the use of the boundary integral equation method, in conjunction with an iteration technique. The numerical calculations have been carried out under the assumption of small-scale yielding. Thus, the equations of the Bodner-Partom model have been used in a region around the crack tip. The conditions on the boundary of this region are provided by the singular term of a corresponding elastic solution. The results show a stress intensity factor which decays with time. At a small distance from the tip the numerically computed normalized opening stress $\tau_{22}(x_1, 0, t)/\tau_{22}(x_1, 0, 0)$ has been compared with a one-term asymptotic representation, i.e., with $K_I(t)/K_I(0)$. The two curves diverge at very small values of time. The inclusion of a second term in the asymptotic expression for the stress gives very acceptable agreement as time increases.

As early as 1971 the boundary integral equation method (BIEM), also called the boundary element method (BEM), was applied by Swedlow and Cruse [8] for elasto-plastic material behavior. In recent years the method has been used extensively for the numerical analyses of viscoelastic/plastic solids of various shapes including bodies containing cracks. Recent work was summarized by Mukherjee [9].

2. Formulation

The states of deformation that will be considered are two-dimensional, either plane or antiplane strain. The body contains a straight crack. At one of the crack tips, say A_1 , the applied loads give rise to elastic stress intensity factors $K_I^E(t)$, $K_{II}^E(t)$ and $K_{III}^E(t)$, if the material were linearly elastic. We will, however, consider a material that displays inelastic behavior as the stress level increases. Hence there will be a domain of inelastic deformation near the crack tip. It is, however, assumed that this domain is small as compared to the crack length, and that linear elasticity applies outside the near-tip domain of inelasticity.

To analyze the field right near the tip A_1 , we follow the arguments that have been introduced for small-scale yielding. Thus, we magnify the geometrical scale near A_1 , so that the geometry becomes one of a semi-infinite crack in a full space, as shown in Fig. 1. A cartesian coordinate system is centered at the crack tip. For the plane strain case, possible boundary conditions on the bounding surfaces of the body are replaced by the asymptotic condition

$$\underline{u} \rightarrow \frac{r^{\frac{1}{2}}}{2\mu} [K_I^E(t) \underline{f}_I(\theta) + K_{II}^E(t) \underline{f}_{II}(\theta)] \quad (2.1)$$

as $r \rightarrow \infty$, where μ is the shear modulus, and (r, θ) are polar coordinates centered at the tip in the magnified configuration. Note that the definition of the stress intensity factors differs from the conventional one by the factor $(2\pi)^{\frac{1}{2}}$. The functions \underline{f}_I and \underline{f}_{II} give the angular variations of the cartesian components of the elastic near tip displacements for modes I and II, i.e.,

$$\underline{\dot{\epsilon}}_I(\theta) = \begin{pmatrix} (\kappa - \frac{1}{2}) \cos\theta/2 - \frac{1}{2} \cos 3\theta/2 \\ (\kappa + \frac{1}{2}) \sin\theta/2 - \frac{1}{2} \sin 3\theta/2 \end{pmatrix} \quad (2.2a)$$

$$\underline{\dot{\epsilon}}_{II}(\theta) = \begin{pmatrix} (\kappa + \frac{3}{2}) \sin\theta/2 + \frac{1}{2} \sin 3\theta/2 \\ (-\kappa + \frac{3}{2}) \cos\theta/2 - \frac{1}{2} \cos 3\theta/2 \end{pmatrix}, \quad (2.2b)$$

where

$$\kappa = \frac{\lambda+3\mu}{\lambda+\mu} \quad (2.3)$$

is a constant in terms of the Lamé's constants λ and μ .

We now proceed to the governing equation for the problem. The strain rate

$$\dot{\underline{\epsilon}} = \frac{\partial \underline{\epsilon}}{\partial t} = \frac{1}{2} [\nabla \underline{u} + (\nabla \underline{u})^T] \quad (2.4)$$

is usually decomposed into the elastic part $\dot{\underline{\epsilon}}^e$ and the inelastic part $\dot{\underline{\epsilon}}^i$ as

$$\dot{\underline{\epsilon}} = \dot{\underline{\epsilon}}^e + \dot{\underline{\epsilon}}^i. \quad (2.5)$$

The elastic part is related to the stress rate $\dot{\underline{\sigma}}$ by Hooke's law,

$$\dot{\underline{\sigma}} = \lambda \text{tr} \dot{\underline{\epsilon}}^e \underline{1} + 2\mu \dot{\underline{\epsilon}}^e, \quad (2.6)$$

where $\underline{1}$ is the unit tensor and "tr" is the 3-D trace. Since the effect of inertia is not considered, the equilibrium equation applies:

$$\nabla \cdot \dot{\mathbf{t}} = 0. \quad (2.7)$$

An equivalent form of (2.7) in terms of the displacement rate $\dot{\mathbf{u}}$ follows from (2.4), (2.5), (2.6) and (2.7) as

$$\Delta_{\mathbf{x}}^* \dot{\mathbf{u}} = \nabla \cdot \dot{\mathbf{g}}^I, \quad (2.8)$$

where

$$\Delta_{\mathbf{x}}^* \dot{\mathbf{u}} = \mu \nabla^2 \dot{\mathbf{u}} + (\lambda + \mu) \nabla \nabla \cdot \dot{\mathbf{u}}, \quad (2.9)$$

and for convenience we have introduced the quantity $\dot{\mathbf{g}}^I$ by

$$\dot{\mathbf{g}}^I = \lambda \text{tr} \dot{\mathbf{e}}^I + 2\mu \dot{\mathbf{e}}^I. \quad (2.10)$$

Equation (2.8) is the governing equation for our problem. This equation, together with the boundary conditions

$$\dot{\mathbf{t}} \cdot \mathbf{n} = 0 \quad \text{on} \quad x_2 = 0^\pm, \quad x_1 < 0, \quad (2.11)$$

and an asymptotic condition of the form (2.1) with \mathbf{u} and $\mathbf{K}_{I,II}^E$ replaced by $\dot{\mathbf{u}}$ and $\dot{\mathbf{K}}_{I,II}^E$, defines $\dot{\mathbf{u}}$. When $\dot{\mathbf{K}}_{I,II}^E = 0$, the behavior of the elastic solution away from the crack tip becomes

$$\dot{\mathbf{u}} \sim O(r^{-1/2}). \quad (2.12)$$

To complete the formulation, we supplement these equations with the regularity requirements at the crack tip:

$$\dot{\mathbf{u}} \sim \text{bounded as } r \rightarrow 0 \quad (2.13)$$

$$\dot{\mathbf{t}} \sim O(1/r) \quad \text{as } r \rightarrow 0 \quad (2.14)$$

In the present problem, we will also discuss the mode-III case, where

$\tau_{\alpha\beta} = \tau_{33} = u_\alpha = 0$ ($\alpha, \beta = 1, 2$). We prefer to use the stress function ϕ because it makes the stress computation easier. The stress function defines the stress components

$$\tau_{\alpha} = \tau_{\alpha 3} \quad (\alpha = 1, 2) \quad (2.15)$$

as

$$\tau_{\alpha} = e_{\alpha\beta} \partial_{\beta} \phi, \quad (2.16)$$

where $e_{\alpha\beta}$ is the permutation symbol.

The compatibility condition

$$e_{\alpha\beta} \partial_{\beta} \dot{\epsilon}_{\alpha} = 0, \quad (\epsilon_{\alpha} = \epsilon_{\alpha 3}) \quad (2.17)$$

together with (2.5), (2.6) and (2.16) yield the governing equation

$$\nabla^2 \dot{\phi} = 2\mu e_{\alpha\beta} \partial_{\alpha} \dot{\epsilon}_{\beta}^i. \quad (2.18)$$

The boundary condition on the crack faces and the regularity condition analogous to (2.14) yield

$$\dot{\phi} = \text{const} \quad (2.19)$$

on the crack faces with the constants for both faces being the same. Also, on the crack line, we have

$$\tau_1 = \partial_2 \phi = 0. \quad (2.20)$$

Finally, the asymptotic condition is

$$\dot{\phi} \rightarrow -2r^{\frac{1}{2}} \dot{K}_{III}^E(t) \cos \frac{1}{2}\theta \quad \text{as } r \rightarrow \infty. \quad (2.21)$$

When $\dot{K}_{III}^E(t) = 0$, (2.21) is replaced by

$$\dot{\phi} \sim O(r^{-\frac{1}{2}}) \quad \text{as } r \rightarrow \infty. \quad (2.22)$$

In this case, the constant in (2.19) is zero because $\dot{\phi}(0) = 0$, as follows from

$$0 = \int_0^{\infty} \dot{\tau}_2 dx_1 = - \int_0^{\infty} \partial_1 \dot{\phi} dx_1 = \dot{\phi}(0) - \dot{\phi}(\infty) = \dot{\phi}(0) \quad (2.23)$$

where (2.22) has been used.

In the sequel, we will consider only the cases where

$$\dot{K}_{I,II,III}^E(t) = 0 . \quad (2.24)$$

3. Representation of the Velocity Field

The term on the right-hand side of the displacement-rate equation (2.8) is of the nature of a body-force distribution. This implies that the solution to Eq.(2.8) can be expressed by the use of a Green's function. Representations in terms of Green's functions are at the basis of the boundary integral equation method (BIEM), and they have therefore become quite well known. For rate-type inelastic analysis the appropriate representations were first developed by Swedlow and Cruse [8]. This Section gives a brief derivation of such representations for the purpose of making the paper self-contained. For further detail we refer to Mukherjee [9] and the papers cited there.

For an unbounded body containing a semi-infinite crack, the Green's function $G(\underline{x}, \underline{y})$ is defined by

$$\Delta_{\underline{x}}^* G(\underline{x}, \underline{y}) = - \frac{1}{2} \delta(\underline{x} - \underline{y}). \quad (3.1)$$

where $\underline{x} = (x_1, x_2)$, $\underline{y} = (y_1, y_2)$, and the operator $\Delta_{\underline{x}}^*$ is defined by (2.9).

On the faces of the crack ($x_1 < 0$, $x_2 = 0^+$) we have

$$T_{\underline{x}} G(\underline{x}, \underline{y}) = 0, \quad (3.2)$$

where $T_{\underline{x}} G$ stands for the elastic tractions computed from G . We also have

$$G(\underline{x}, \underline{y}) \sim O(\log |\underline{x}|) \quad \text{as } |\underline{x}| \rightarrow \infty, \quad (3.3)$$

$$G(\underline{x}, \underline{y}) \sim O(1) \quad \text{as } |\underline{x}| \rightarrow 0, \quad (3.4)$$

$$\nabla_{\underline{x}} G(\underline{x}, \underline{y}) \sim O(1/\sqrt{|\underline{x}|}) \quad \text{as } |\underline{x}| \rightarrow 0. \quad (3.5)$$

A standard analysis based on Muskhelishvili's method yields $G(\underline{x}, \underline{y})$ as

$$\begin{pmatrix} G_{11} + i & G_{21} \\ G_{12} + i & G_{22} \end{pmatrix} = \frac{1}{2\pi\mu(1+\kappa)} \begin{pmatrix} 1 \\ i \end{pmatrix} \left\{ \frac{(\bar{z}_0 - z_0)(z - \bar{z})}{4\sqrt{z}\sqrt{z_0}(\sqrt{z_0} + \sqrt{z})^2} - \kappa \log(\sqrt{z} - \sqrt{z_0})(\sqrt{z} - \sqrt{\bar{z}_0}) \right. \\ \left. - \kappa^2 \log(\sqrt{z} + \sqrt{\bar{z}_0}) - \log(\sqrt{z} + \sqrt{z_0}) \right\}$$

$$+ \left(\frac{1}{-i} \right) \left\{ \frac{\kappa}{2} \left(\frac{z_0 - \bar{z}_0}{\sqrt{z_0}(\sqrt{z_0} + \sqrt{\bar{z}_0})} + \frac{z - \bar{z}}{\sqrt{z}(\sqrt{z_0} + \sqrt{\bar{z}_0})} \right) + \frac{1}{2(\bar{z} - \bar{z}_0)} \left(z - z_0 + \frac{z\bar{z}_0 - z_0\bar{z}}{\sqrt{z}\sqrt{z_0}} \right) \right\} \quad (3.6)$$

where κ is defined by (2.3), and

$$z = x_1 + ix_2, \quad z_0 = y_1 + iy_2. \quad (3.7)$$

Equation (3.6) agrees with the expressions given by Erdogan [10].

A suitable representation of the solution to (2.8) is obtained by the use of Green's identity:

$$\int_{A_{R,\epsilon}} (\Delta_{\bar{x}}^* \bar{v}) \cdot \bar{w} \, dA_{\bar{x}} - \int_{A_{R,\epsilon}} (\Delta_{\bar{x}}^* \bar{w}) \cdot \bar{v} \, dA_{\bar{x}} = \int_{\partial A_{R,\epsilon}} (T_{\bar{x}} \bar{v}) \cdot \bar{w} \, dc - \int_{\partial A_{R,\epsilon}} (T_{\bar{x}} \bar{w}) \cdot \bar{v} \, dc, \quad (3.8)$$

which holds for an arbitrary pair (\bar{v}, \bar{w}) , and where $A_{R,\epsilon}$ is the domain bounded by circles of radii ϵ and R ($0 < \epsilon < R$) centered at the tip, and by the crack faces, as shown in Fig. 2.

We now substitute $\dot{\bar{u}}(\bar{x})$ for $\bar{v}(\bar{x})$ and $\bar{G}(\bar{x}, \bar{y})$ for $\bar{w}(\bar{x})$ in (3.8). Subsequent use of the divergence theorem and the regularity conditions (2.13), (2.14), (3.4) and (3.5), followed by letting $R \rightarrow \infty$, $\epsilon \rightarrow 0$, and using (2.12) and (3.3), gives

$$\dot{\bar{u}}(\bar{x}, t) = \int_{R^2} \nabla_{\bar{y}} \bar{G}(\bar{y}, \bar{x}) \cdot \dot{\bar{g}}^i(\bar{y}, t) dA_{\bar{y}}, \quad (3.9)$$

or in component form

$$\dot{u}_j(\bar{x}, t) = \int_{R^2} \nabla_{y_k} G_{kj}(\bar{y}, \bar{x}) \dot{g}_{lk}^i(\bar{y}, t) dA_{\bar{y}}. \quad (3.10)$$

In deriving these equations we have assumed that the integrals in (3.9) or (3.10) converge. For this to be true, it is sufficient to assume that \dot{g}^i satisfies

$$|\dot{g}^1| \sim O(r^{\alpha_1}) \quad \text{as } r \rightarrow 0. \quad (3.11)$$

$$|\dot{g}^1| \sim O(r^{\alpha_2}) \quad \text{as } r \rightarrow \infty \quad (3.12)$$

with

$$\alpha_1 > -1, \quad \alpha_2 < -1. \quad (3.13a,b)$$

Although (3.13a) appears unnecessarily restrictive, it turns out that these inequalities guarantee the satisfaction of the conditions (2.13) and (2.14) automatically. It is noted, however, that (3.13) is just a sufficient condition.

For the Mode III case a similar procedure gives

$$\dot{\phi}(\underline{x}, t) = \int_{R^2} \partial_{y_j} G(\underline{y}, \underline{x}) e_{jk} \dot{\phi}_k^1(\underline{y}, t) dA_y \quad (3.14)$$

where

$$G(\underline{x}, \underline{y}) = -\frac{1}{4\pi} \log \frac{(\sqrt{z} - \sqrt{z_0})(\sqrt{\bar{z}} - \sqrt{\bar{z}_0})}{(\sqrt{z} + \sqrt{z_0})(\sqrt{\bar{z}} + \sqrt{\bar{z}_0})}. \quad (3.15)$$

Hence we have

$$\dot{\phi}_p(\underline{x}, t) = e_{pq} \partial_{x_q} \int_{R^2} \partial_{y_j} G(\underline{y}, \underline{x}) e_{jk} \dot{\phi}_k^1(\underline{y}, t) dA_y. \quad (3.16)$$

4. Asymptotic Expansions

In the following sections, we employ the potential representation for \dot{u} given in Section 3. The results of this section are analytical, while numerical results are presented in Section 7.

For a certain class of constitutive models the quantity \dot{q}^1 , given by Eq.(2.10), is finite. For example, a viscoplastic model proposed by Bodner and Partom [1] shows this property. In this section we will obtain the asymptotic expression for \dot{u} for the case that $\lim_{r \rightarrow 0} \dot{q}^1(r, \theta, t)$ exists for all θ .

In a conventional asymptotic analysis one seeks near-tip fields of the forms

$$\dot{u} = \dot{u}_1 + \dot{u}_2 + \dot{u}_3 + \dots \quad (4.1)$$

$$\dot{q}^1 = \dot{q}_1^1 + \dot{q}_2^1 + \dot{q}_3^1 + \dots \quad (4.2)$$

where \dot{u}_j, \dot{q}_j^1 ($j = 1, \dots$) are functions which are less singular near $r = 0$ with increasing subscript. Since near $r = 0$

$$\dot{q}^1 = \dot{q}^1(0, \theta, t) + o(1) \quad (4.3)$$

is bounded, and

$$\nabla \cdot \dot{q}_1^1 = \frac{1}{r} \bar{q}(\theta, t), \quad (4.4)$$

we find by substituting (4.1) and (4.2) into (2.8)

$$\Delta^* \dot{u}_1 = 0 \quad (4.5)$$

$$\Delta^* \dot{u}_2 - \nabla \cdot \dot{g}_1^1 = 0 \quad (4.6)$$

Equation (4.5) implies that \dot{u}_1 is of the same form as for the linearly elastic case. The appropriate separation of variables form of (4.6) can only be guessed at this stage. One might try

$$\dot{u}_2 = r \bar{f}(\theta, t) \quad (4.7)$$

This expression for $\bar{f}(\theta, t)$ does, however, not lead to a solution of (4.6) because the corresponding homogeneous problem has nontrivial solutions. In the Mode I case, for example, the homogeneous equation

$$\Delta^*[r \bar{f}(\theta, t)] = 0, \quad (4.8)$$

with boundary conditions

$$\theta = \pi: \quad T[r \bar{f}(\theta, t)] = 0 \quad (4.9)$$

$$\theta = 0: \quad i_1 \cdot T[r \bar{f}(\theta, t)] = 0 \text{ and } i_2 \cdot [r \bar{f}(\theta, t)] = 0, \quad (4.10a, b)$$

where i_j are unit vectors, has a solution corresponding to a uniaxial tensile field in the x_1 direction. Hence the approach based on (4.7) becomes ambiguous at this point.

An unequivocal form of the term \dot{u}_2 can, however, be obtained directly from the representation given by (3.10). Using polar coordinates (r, θ) and (r_o, θ_o) for y and x , we split (3.9) into two integrals as

$$\begin{aligned} \dot{u}(r_o, \theta_o, t) = & \int_{-\pi}^{\pi} \int_0^{r_o} r \nabla G_{<}(r, \theta; r_o, \theta_o) \cdot \dot{g}^1(r, \theta, t) dr d\theta \\ & + \int_{-\pi}^{\pi} \int_{r_o}^{\infty} r \nabla G_{>}(r, \theta; r_o, \theta_o) \cdot \dot{g}^1(r, \theta, t) dr d\theta \end{aligned} \quad (4.11)$$

Here the gradient operator is taken with respect to the polar coordinates r and θ . Next $\nabla G_{<}$ and $\nabla G_{>}$ are expanded into power series of r . We can write

$$r < r_0: \quad r \nabla G_{<} = \sum_{n=0}^{\infty} \left(\frac{r}{r_0}\right)^{\frac{n+1}{2}} M_{n+1}(\theta, \theta_0) \quad (4.12)$$

$$r > r_0: \quad r \nabla G_{>} = \sum_{n=-1}^{\infty} \left(\frac{r_0}{r}\right)^{\frac{n+1}{2}} N_{n+1}(\theta, \theta_0) \quad (4.13)$$

The coefficients in (4.12)-(4.13) can be obtained from (3.6). It is found that N_0 is independent of θ_0 .

Substitution of (4.12)-(4.13) into (4.11) yields after some rearrangements

$$\dot{q}(r_0, \theta_0) = \dot{f}_0 + \dot{f}_1(\theta_0) r_0^{\frac{1}{2}} + \dot{i}_{<}(r_0, \theta_0) + \dot{i}_{>}(r_0, \theta_0) \quad (4.14)$$

where

$$\dot{f}_0 = \int_{-\pi}^{\pi} \int_0^{\infty} N_0(\theta) \cdot \dot{q}^1(r, \theta) dr d\theta \quad (4.15)$$

$$\dot{f}_1(\theta_0) = \int_{-\pi}^{\pi} \int_0^{\infty} r^{\frac{1}{2}} N_1(\theta, \theta_0) \cdot \dot{q}^1(r, \theta) dr d\theta \quad (4.16)$$

$$\dot{i}_{<}(r_0, \theta_0) = \int_{-\pi}^{\pi} \left\{ \int_0^{r_0} \left[\sum_{n=0}^{\infty} \left(\frac{r}{r_0}\right)^{\frac{n+1}{2}} M_{n+1}(\theta, \theta_0) \right] - N_0(\theta) - N_1(\theta, \theta_0) \left(\frac{r_0}{r}\right)^{\frac{1}{2}} \right\} \cdot \dot{q}^1(r, \theta) dr d\theta \quad (4.17)$$

$$\dot{i}_{>}(r_0, \theta_0) = \int_{-\pi}^{\pi} \left[\int_{r_0}^{\infty} \sum_{n=1}^{\infty} \left(\frac{r_0}{r}\right)^{\frac{n+1}{2}} N_{n+1}(\theta, \theta_0) \right] \cdot \dot{q}^1(r, \theta) dr d\theta \quad (4.18)$$

The dependence on time t , shown in (4.11) is implied, but not explicitly shown in (4.14)-(4.18) and in the sequel. In the next step the orders in r_0 of the integrals (4.17) and (4.18) are determined.

Since $\dot{q}^1(r, \theta)$ has an estimate given by (4.3) it follows that (4.17) is of order r_0 , i.e.,

$$\dot{f}_<(r_0, \theta_0) = r_0 \dot{A}(\theta_0) + o(r_0) \quad (4.19)$$

where

$$\dot{A}(\theta_0) = \int_{-\pi}^{\pi} \left\{ \left[\sum_{n=0}^{\infty} \frac{2}{n+3} M_{n+1}(\theta, \theta_0) \right] - N_0(\theta) - 2 N_1(\theta, \theta_0) \right\} \cdot \dot{q}^1(0, \theta) d\theta \quad (4.20)$$

A discussion of the order of the integral in (4.18) is given in Appendix A.

The result is

$$\dot{f}_>(r_0, \theta_0) = \dot{f}_2(\theta_0) r_0 \log r_0 + r_0 \dot{B}(\theta_0) + o(r_0) \quad (4.21)$$

where

$$\dot{f}_2(\theta_0) = - \int_{-\pi}^{\pi} N_2(\theta, \theta_0) \cdot \dot{q}^1(0, \theta) d\theta \quad (4.22)$$

The function $\dot{B}(\theta_0)$ is defined by Eq. (A.6). By combining (4.14), (4.19) and (4.21) it is concluded that $\dot{u}(r_0, \theta_0)$ is of the form

$$\dot{u}(r_0, \theta_0) = \dot{f}_0 + \dot{f}_1(\theta_0) r_0^{\frac{1}{2}} + \dot{f}_2(\theta_0) r_0 \log r_0 + \dot{f}_3(\theta_0) r_0 + o(r_0) \quad (4.23)$$

where

$$\dot{f}_3(\theta_0) = \dot{A}(\theta_0) + \dot{B}(\theta_0) \quad (4.24)$$

The constant \dot{f}_0 in (4.23) corresponds to a rigid-body motion; it will be left out from further considerations. Some additional manipulations reduces $\dot{f}_1(\theta_0)$ and $\dot{f}_2(\theta_0)$ to the forms

$$\dot{f}_1(\theta_0) = [\dot{K}_{II} \dot{f}_{II}(\theta_0) + \dot{K}_{II} \dot{f}_{II}(\theta_0)] / 2\mu, \quad (4.25)$$

$$\dot{f}_2(\theta_o) = \dot{L}_I \begin{pmatrix} (\kappa+1)\cos\theta \\ (\kappa-3)\sin\theta \end{pmatrix} + \dot{L}_{II} \begin{pmatrix} \sin\theta \\ -\cos\theta \end{pmatrix}, \quad (4.26)$$

where $\dot{f}_I(\theta_o)$ and $\dot{f}_{II}(\theta_o)$ are defined by (2.2a,b), and

$$\dot{K}_{I,II}(t) = \frac{1}{2\pi(\kappa+1)} \int_{-\pi}^{\pi} \int_0^{\infty} r^{-\frac{1}{2}} D_{I,II} \cdot \dot{g}^1(r, \theta, t) dr d\theta, \quad (4.27)$$

Also

$$\dot{L}_{I,II}(t) = -\frac{1}{8\pi\mu(\kappa+1)} \int_{-\pi}^{\pi} E_{I,II} \cdot \dot{g}^1(0, \theta, t) d\theta, \quad (4.28)$$

In (4.27)-(4.28)

$$D_I = \begin{pmatrix} (\kappa - \frac{5}{2})\cos\frac{3\theta}{2} + \frac{3}{2}\cos\frac{7\theta}{2}, & -\frac{3}{2}\sin\frac{3\theta}{2} + \frac{3}{2}\sin\frac{7\theta}{2} \\ -\frac{3}{2}\sin\frac{3\theta}{2} + \frac{3}{2}\sin\frac{7\theta}{2} & (\kappa + \frac{1}{2})\cos\frac{3\theta}{2} - \frac{3}{2}\cos\frac{7\theta}{2} \end{pmatrix}, \quad (4.29a)$$

$$D_{II} = \begin{pmatrix} -(\kappa - \frac{1}{2})\sin\frac{3\theta}{2} - \frac{3}{2}\sin\frac{7\theta}{2}, & \frac{1}{2}\cos\frac{3\theta}{2} + \frac{3}{2}\cos\frac{7\theta}{2} \\ \frac{1}{2}\cos\frac{3\theta}{2} + \frac{3}{2}\cos\frac{7\theta}{2} & -(\kappa - \frac{3}{2})\sin\frac{3\theta}{2} + \frac{3}{2}\sin\frac{7\theta}{2} \end{pmatrix}, \quad (4.29b)$$

$$E_I = \begin{pmatrix} (1 - \kappa)\cos 2\theta - 2\cos 4\theta, & -2\sin 4\theta \\ -2\sin 4\theta & (1 - \kappa)\cos 2\theta + 2\cos 4\theta \end{pmatrix}, \quad (4.30a)$$

$$E_{II} = (1 + \kappa) \begin{pmatrix} (\kappa - 3)\sin 2\theta + 2\sin 4\theta, & 2(\cos 2\theta - \cos 4\theta) \\ 2(\cos 2\theta - \cos 4\theta) & (\kappa - 3)\sin 2\theta - 2\sin 4\theta \end{pmatrix}. \quad (4.30b)$$

It is shown in Appendix A that $\dot{f}_3(\theta)$ can be written in the form

$$\dot{f}_3(\theta_o) = \int_{-\pi}^{\pi} P(\theta; \theta_o) \cdot \dot{g}^1(0, \theta) d\theta + \dot{c}_1 \begin{pmatrix} (\kappa+1)\cos\theta_o \\ (\kappa-3)\sin\theta_o \end{pmatrix} + \dot{c}_2 \begin{pmatrix} \sin\theta_o \\ -\cos\theta_o \end{pmatrix} \quad (4.31)$$

The function $P(\theta; \theta_o)$ is complicated. For the Mode I case we find after lengthy manipulations

$$\begin{aligned}
\dot{\underline{\underline{f}}}_3(\theta_0) = & - \int_0^\pi \left[\frac{\partial}{\partial \theta} \underline{\underline{F}}(\theta; \theta_0) \left(1 - \frac{2}{1+\kappa} \underline{\underline{l}}' \times \underline{\underline{l}}' \right) \dot{\underline{\underline{q}}}^1(0, \theta) \underline{\underline{l}}' d\theta - \right. \\
& \frac{2}{1+\kappa} \int_0^\pi \underline{\underline{F}}(\theta; \theta_0) (\underline{\underline{l}} \times \underline{\underline{l}}' + \underline{\underline{l}}' \times \underline{\underline{l}}) \dot{\underline{\underline{q}}}^1(0, \theta) \underline{\underline{l}}' d\theta + \int_0^\pi \underline{\underline{F}}(\theta; \theta_0) \left(1 - \frac{2}{1+\kappa} \underline{\underline{l}}' \times \underline{\underline{l}}' \right) \\
& \dot{\underline{\underline{q}}}^1(0, \theta) \underline{\underline{l}} d\theta - 2 \dot{\underline{\underline{I}}}_T \mu \int_0^\pi \underline{\underline{F}}(\theta; \theta_0) (\underline{\underline{g}}(\theta) + 2\underline{\underline{l}}) d\theta - \\
& \left. (3-\kappa) \dot{\underline{\underline{I}}}_T \mu \begin{pmatrix} 0 \\ \sin \theta_0 \end{pmatrix} + C \underline{\underline{g}}(\theta_0) \right] \quad (4.32)
\end{aligned}$$

where C is a constant, and

$$\underline{\underline{F}}(\theta; \theta_0) = \begin{pmatrix} \cos(\min(\theta, \theta_0)) \sin(\max(\theta, \theta_0)) & 0 \\ 0 & -\sin(\min(\theta, \theta_0)) \cos(\max(\theta, \theta_0)) \end{pmatrix} \quad (4.33)$$

Also

$$\underline{\underline{l}} = \begin{pmatrix} \cos \theta \\ \sin \theta \end{pmatrix}, \quad \underline{\underline{l}}' = \begin{pmatrix} -\sin \theta \\ \cos \theta \end{pmatrix} \quad (4.34a, b)$$

$$\underline{\underline{g}}(\theta) = \begin{pmatrix} (\kappa+1) \cos \theta \\ (\kappa-3) \sin \theta \end{pmatrix} \quad (4.34c)$$

The symbol \times defines a product of a column and a row vector. For example

$$\underline{\underline{l}} \times \underline{\underline{l}}' = \begin{bmatrix} \cos \theta \\ \sin \theta \end{bmatrix} \begin{bmatrix} -\sin \theta & \cos \theta \end{bmatrix} = \begin{bmatrix} -\cos \theta \sin \theta & \cos^2 \theta \\ -\sin^2 \theta & \cos \theta \sin \theta \end{bmatrix} \quad (4.35)$$

Equation (4.23) implies that the dominant singularity of the strain rate has exactly the same form as in linear elasticity. The rates of the stress intensity factors $\dot{K}_{I,II}$ are given by (4.27). The second singular term, is of the order of $\log r$ near the tip. The magnitude of the multiplying term is determined only by the distribution of \dot{q}^1 at the tip. Because of this last

property, the expression (4.28) holds true for any crack configuration, whereas (4.27) is true only in the sense of the "small-scale yielding". The logarithmic singularity in the strain rate does not give rise to a logarithmic stress singularity except in τ_{11} for mode I.

For the mode III case, we can use the same general approach to show that

$$\dot{\underline{t}} = \frac{\dot{K}_{III}(t)}{\sqrt{r}} \begin{pmatrix} -\sin\frac{\theta}{2} \\ \cos\frac{\theta}{2} \end{pmatrix} + \dot{\underline{h}}(\theta), \quad (4.36)$$

where

$$\dot{K}_{III} = \frac{1}{4\pi} \int_{-\pi}^{\pi} d\theta \int_0^{\infty} [-\dot{\sigma}_1^I(r, \theta) \sin\frac{3\theta}{2} + \dot{\sigma}_2^I(r, \theta) \cos\frac{3\theta}{2}] r^{-\frac{1}{2}} dr \quad (4.37)$$

$$\begin{aligned} \dot{\underline{h}}(\theta_0) = & \begin{pmatrix} 1 \\ 0 \end{pmatrix} \int_0^{\theta_0} [\underline{l}' \cdot \dot{\underline{\sigma}}^I(0, \theta) \cos\theta - \underline{l} \cdot \dot{\underline{\sigma}}^I(0, \theta) \sin\theta] d\theta \\ & - \begin{pmatrix} 0 \\ 1 \end{pmatrix} \int_{\theta_0}^{\pi} [\underline{l}' \cdot \dot{\underline{\sigma}}^I(0, \theta) \sin\theta + \underline{l} \cdot \dot{\underline{\sigma}}^I(0, \theta) \cos\theta] d\theta \\ & - [\underline{l} \cdot \dot{\underline{\sigma}}^I(0, \theta_0)] \underline{l} \end{aligned} \quad (4.38)$$

Note that the stress rate and hence the strain rate do not have logarithmic singularities. As for the mode I case, we can relate the absence of the logarithmic term either to the non existence of a non-trivial solution to a certain boundary value problem or to the lack of a certain term in the far field expansion of the Green's function.

In the published literature, the choice of terms for asymptotic expansions is generally made on a trial and error basis. The analysis presented in this section gives a more rational foundation to asymptotic near-tip.

5. . The Bodner-Partom Model

In Ref.[1], Bodner and Partom proposed a set of constitutive equations for an elastic-viscoplastic material. These equations have the convenient property that no separate specification of a yield criterion is required, nor is it necessary to consider loading and unloading separately. Within the context of the Bodner-Partom model both elastic and inelastic deformations are present at all stages of loading and unloading, but the inelastic deformations are very small at low stress levels. The Bodner-Partom equations have been used to model the mechanical behavior of several metals over a wide range of temperatures and strain rates. Very satisfactory agreement between theoretical and experimental results has generally been obtained. For a recent discussion of the Bodner-Partom model we refer to Ref.[12].

The constitutive equations follow by supplementing Eqs.(2.5) and (2.6) with an expression for the rate of inelastic strain. In a recent version of the Bodner-Partom theory this strain rate is given by, see [12],

$$\dot{\epsilon}^I = D_0 \frac{\tau'}{\sqrt{J_2}} \exp[-(Z^2/3J_2)^n/2], \quad (5.1)$$

where τ' is the stress deviator

$$\tau' = \tau - \frac{1}{3} \frac{1}{\tau} \text{tr} \tau, \quad (5.2)$$

and

$$J_2 = \frac{1}{2} \tau' \cdot \tau'. \quad (5.3)$$

Also

$$Z = Z_1 + (Z_0 - Z_1)e^{-mW_p} \quad (5.4)$$

In (5.1) and (5.4), Z_0 , Z_1 , m , n and D_0 are material constants, while W_p is the work over the inelastic strains,

$$W_p = \int \tau \cdot \dot{\epsilon}^i dt. \quad (5.5)$$

For uniaxial tension it is simple to plot the inelastic strain rate versus σ/Z . For various values of n the curves are shown in Fig. 3. The linear plot of Fig. 3 shows that $\dot{\epsilon}^i$ remains very small at small stresses with a rapid change over a small range of σ/Z (the "yield" region), and that an asymptotic limit is approached as σ becomes large.

It is of interest to note that the components of $\dot{\epsilon}^i$, as defined by Eq.(5.1), are always bounded. Even if τ is singular (which is the case at a crack tip), the singularity of τ as $r \rightarrow 0$ will be cancelled by the singularity of $\sqrt{J_2}$ in the term $\tau'/\sqrt{J_2}$. The term $\exp[-(Z^2/3J_2)^{n/2}]$ is bounded whether J_2 is singular or not. Hence Eq.(5.1) implies that the inelastic strain rate is bounded at a crack tip. It then follows from Eq.(2.10) that the components of \dot{q}^i are also bounded at a crack tip, and it can thus be concluded that the asymptotic results of Section 4 apply to the Bodner-Partom model.

6. Numerical Procedure

A numerical procedure has been developed to compute the stress intensity factor and the opening stress τ_{22} at a position on the crack line. As pointed out by Mukherjee and co-workers [13], a numerical evaluation based on the representation (3.9) is very efficient for viscoplastic problems and for viscoelastic problems of the Maxwell model type. Here we use this approach (generally referred to as the BIE method) for crack tip fields governed by the Bodner-Partom equations. The procedure proceeds as follows

1) Compute the initial field. Since the inelastic strain is zero at $t = 0$, the initial field is simply the linearly elastic one. In the present context this field is

$$u|_{t=0} = \frac{\sqrt{r}}{2\mu} [K_{I}^E f_I(\theta) + K_{II}^E f_{II}(\theta)] \quad (6.1)$$

Hence, the solution is known for $t = n\Delta t$ with $n = 0$, where Δt is the time increment.

2) Subdivide the near-tip domain into cells, and compute $\dot{\xi}^i$ at the centroid of each cell by using (5.1). Then assuming that $\dot{\xi}^i$ may be taken as constant over each cell, \dot{u} is computed by using (3.9) and $\nabla \dot{u}$ by differentiating (3.9).

3) Compute $\dot{\tau}$ from (2.5) and (2.6). Update τ by using

$$\tau[(n+1)\Delta t] = \tau(n\Delta t) + \Delta t \dot{\tau}(n\Delta t). \quad (6.2)$$

4) Use the updated value of τ to compute $\dot{\xi}^i$ as in 2), and repeat 2) and 3).

When the edges of the cells are straight, the integrals involved in

(3.9) can be evaluated analytically, as discussed by Cruse and Polch [11]. By picking up the square-root singular terms in these integrals and summing up their coefficients, $\dot{K}_{I,II}$ can be computed. Alternatively, the computation of $\dot{K}_{I,II}$ may be carried out by using (4.27) with the piecewise constant approximation for $\dot{\epsilon}^p$.

7. Numerical Results

Numerical computations have been carried out for the non-hardening case of the Bodner-Partom model. With reference to Eqs.(5.1) and (5.4), this case corresponds to

$$Z_0/Z_1 = 1 \quad (7.1)$$

It is then convenient to introduce non-dimensional quantities as follows

$$\bar{u} = u (\mu Z/\sqrt{3}) / (K_I^E)^2, \quad \bar{\tau} = \tau / (Z/\sqrt{3}) \quad (7.2a,b)$$

$$\bar{x} = x (Z^2/3) / (K_I^E)^2, \quad \bar{t} = t (\mu D_0) / (Z/\sqrt{3}) \quad (7.3a,b)$$

$$\dot{\bar{e}} = \frac{d\bar{e}}{d\bar{t}} / D_0 \quad (7.4)$$

Here the dot notation represents the derivative with respect to \bar{t} . In terms of these dimensionless quantities, Eqs.(5.1), (2.6) and (2.8) convert into

$$\dot{\bar{e}}^i = [\bar{\tau}' / (\frac{1}{2}\bar{\tau}' \cdot \bar{\tau}')^{1/2}] \exp[-\frac{1}{2}(\frac{1}{2}\bar{\tau}' \cdot \bar{\tau}')^{-n}] \quad (7.5)$$

$$\dot{\bar{\tau}} = \frac{\lambda}{\mu} (\bar{\nabla} \cdot \dot{\bar{u}}) \bar{1} + \bar{\nabla} \dot{\bar{u}} + (\bar{\nabla} \dot{\bar{u}})^T - 2\dot{\bar{e}}^i \quad (7.6)$$

$$\bar{\nabla}^2 \dot{\bar{u}} + \frac{\lambda+\mu}{\mu} \bar{\nabla} \bar{\nabla} \cdot \dot{\bar{u}} = 2\bar{\nabla} \cdot \dot{\bar{e}}^i, \quad (7.7)$$

where $\bar{\nabla}$ and $\bar{\nabla}^2$ are the del operator and the Laplacian with respect to the dimensionless optical coordinates \bar{x}_1 , and $\bar{\tau}'$ is the dimensionless stress deviator. Since λ/μ and $(\lambda+\mu)/\mu$ can be expressed in terms of the elastic Poisson's ratio, ν , it now follows that numerical values have to be chosen only for ν and n . Here we choose

$$n = 1, \text{ and } \nu = 0.2 \quad (7.8)$$

For the numerical procedure based on the boundary integral equation method described in Section 6, the cell arrangement shown in Fig. 4 has been used. The expression for the time rate of change of the stress intensity factor is given by Eq.(4.27). Once the inelastic strain rate has been computed, the term $\dot{\sigma}_1^1$ can be determined and (4.27) can be evaluated numerically. A subsequent numerical integration with respect to time produces $K_I(t)$. Figure 5 shows $K_I(\bar{t})/K_I^E$ versus the dimensionless time \bar{t} . It is noted that $K_I(\bar{t})/K_I^E$ decreases with time. Also shown in Fig. 5 is the normalized stress $\tau_{22}(\bar{x}_1, 0, \bar{t})/\tau_{22}(\bar{x}_1, 0, 0)$, evaluated at $\bar{x}_1 = 0.0014$. The two curves diverge rapidly as the dimensionless time increases.

It is instructive to compute the actual physical distance to the crack tip which would correspond to $\bar{x}_1 = 0.0014$. Suppose we consider a crack in an unbounded medium under far-field uniform tension $\tau_{22} = \sigma_o$. Then $K_I^E = \sigma_o \sqrt{(\pi a)}$. For titanium, Ref.[1] suggests the following value for the yield stress, $\sigma_Y \sim 250 \text{ N/mm}^2$, while $Z \sim 1200 \text{ N/mm}^2$. Let $\sigma_o \sim \sigma_Y/2$. Equation (7.3a) then yields $x_1 \sim 0.102a\bar{x}_1$. Hence $\bar{x}_1 = 0.0014$ corresponds to $x_1 \sim 1.428 \times 10^{-4} a$, which is a very short distance to the crack tip. The two curves in Fig. 5 thus imply that even very close to the crack tip, the singular term by itself would give a very poor approximation to the near-tip stress τ_{22} , with an error which increases with time \bar{t} . The relation between physical time t and dimensionless time \bar{t} can be obtained from (7.3b) as $\bar{t} = .635 \times 10^6 t$, where the following values from Ref.[1] have been used $D_o \sim 10^4/\text{sec}$ and $\mu = .44 \times 10^5 \text{ N/mm}^2$. As predicted by the constitutive model

used in this paper, the relaxation of the stress intensity factor takes place very rapidly.

An improved asymptotic representation of the near-tip stresses can be obtained by including higher order terms. The calculation of these terms requires the evaluation of the integrals for \dot{L}_I , Eq.(4.28), and $\dot{f}_3(\theta_0)$, Eq.(4.32). The $r \log r$ term in Eq.(4.23) contributes only a constant term to $\dot{\tau}_{22}$. A constant contribution is also obtained from the term $\dot{f}_3(\theta_0)r_0$. After the calculations have been completed we find on the crack line ($\theta = 0$)

$$\dot{\tau}_{22} \sim \frac{\bar{K}(\bar{t})}{\sqrt{\bar{F}}} - 3.376 \quad (7.9)$$

or

$$\tau_{22} \sim \frac{\bar{K}(\bar{t})}{\sqrt{\bar{F}}} - 3.376\bar{t} \quad (7.10)$$

This two term expansion gives excellent agreement with the numerical result, as can be seen from the numerical values listed in Table 1.

Figure 6 shows $K_{III}(\bar{t})/K_{III}^E$ versus the dimensionless time \bar{t} . Also shown is the ratio $T_2(\bar{x}_1, 0, \bar{t})/T_2(\bar{x}_1, 0, 0)$ evaluated at $\bar{x}_1 = 0.0047$. As for the Mode I case, the two curves diverge rapidly as \bar{t} increases.

It is relatively simple to write out explicitly the asymptotic results for the Mode III case. At the crack tip we obtain from Eq.(7.5)

$$\dot{\bar{E}}^I(0, \theta) = \begin{pmatrix} -\sin \frac{1}{2}\theta \\ \cos \frac{1}{2}\theta \end{pmatrix} \quad (7.11)$$

Use of this result in (4.36)-(4.38), and subsequent integration with respect to time yields

$$\tau_2 = \frac{\bar{K}_{III}(\bar{t})}{\sqrt{\bar{r}}} \begin{pmatrix} -\sin \frac{\theta}{2} \\ \cos \frac{\theta}{2} \end{pmatrix} + \frac{1}{3} \bar{t} \begin{pmatrix} \sin \frac{3\theta}{2} + 3 \sin \frac{\theta}{2} \\ -\cos \frac{3\theta}{2} - 3 \cos \frac{\theta}{2} \end{pmatrix} \quad (7.12)$$

The values of τ_2 at $\bar{x}_1 = 0.0047$, $\bar{x}_2 = 0$ computed according to Eq.(7.12) and by the BIEM have been listed in Table 1. Good agreement is observed.

The results presented in this section show that the square root singular term presents a very poor approximation to the crack tip field even at very small distances from the crack tip. The approximation becomes worse as time increases. The use of additional terms in the asymptotic expression for the particle velocity provides, however, a very satisfactory agreement over the whole range of time between the corresponding asymptotic representation and the numerically computed stress component at a crack-line point just ahead of the crack tip.

Acknowledgment

This work was carried out in the course of research sponsored by the U.S. Office of Naval Research (Contract No. N00014-76-C-0063).

References

1. Bodner, S.R. and Partom, Y., "Constitutive Equations for Elastic-Viscoplastic Strain-Hardening Materials", J. Appl. Mech., 42, pp. 385-389, 1975.
2. Riedel, H., "Cracks Loaded in Anti-Plane Shear Under Creep Conditions", Zeitschrift für Metall Kunde, Vol. 69, No. 12, pp. 755-760, 1978.
3. Riedel, H. and Rice, J.R., "Tensile Cracks in Creeping Solids", Fracture Mechanics (Proceedings of the 12th National Symposium on Fracture Mechanics, St. Louis, May 1979) (edited by P. C. Paris), ASTM STP 700, pp. 112-130, American Society for Testing and Materials, Philadelphia.
4. Hui, C.Y. and Riedel, H., "The Asymptotic Stress and Strain Field Near the Tip of a Growing Crack under Creep Conditions", Int. J. of Fracture, Vol. 17, No. 4, pp. 409-425, 1981.
5. Lo, K.K., "Dynamic Crack-Tip Fields in Rate-Sensitive Solids", J. Mech. Phys. Solids, Vol. 31, No. 4, pp. 287-305, 1983.
6. Hart, E.W., "A Theory for Stable Crack Extension Rates in Ductile Materials", Int. J. Solids Structures, Vol. 16, pp. 807-823, 1980.
7. Freund, L.B. and Hutchinson, J.W., "High Strain-Rate Crack Growth in Rate-Dependent Plastic Solids", J. Mech. Phys. Solids, Vol. 33, No. 2, pp. 169-191, 1985.
8. Swedlow, J.L. and Cruse, T.A., "Formulation of Boundary-Integral Equations for Three-Dimensional Elastoplastic Flow", Int. J. Solids Structures 7, pp. 1673-1683, 1971.

9. Mukherjee, S., Boundary Element Methods in Creep and Fracture, Applied Science Publisher, London, 1982.
10. Erdogan, F., "On the Stress Distribution in Plates with Collinear Cuts under Arbitrary Loads", Proceedings of 4th U.S. National Congress of Applied Mechanics, Edited by R.M. Rosenberg, pp. 547-553, 1962.
11. Cruse, T.A. and Polch, E.Z., "Elastoplastic BIE Analysis of Cracked Plates and Related Problems", to be published.
12. Bodner, S.R., "Review of a Unified Elasto-Viscoplastic Theory," Interim Scientific Report, October, 1984, prepared for the Air Force Office of Scientific Research, Bolling AFB, D.C. 20332.
13. Mukherjee, S. and Kumar, V., "Numerical Analysis of Time-Dependent Inelastic Deformation in Metallic Media Using the Boundary-Integral Equation Method," J. Appl. Mech., Vol. 45, pp. 785-790, 1978.
14. Kanwal, R.P., Generalized Functions: Theory and Technique, Academic Press, pp. 75-104, 1983.

Appendix A: Finite Parts of Integrals

The "finite part" of an integral, denoted by pf, is defined as (see [14], pp. 75-104)

$$\text{pf} \int_0^{\infty} f(x) dx = \lim_{\substack{R \rightarrow \infty \\ \epsilon \rightarrow 0}} \left[\int_{\epsilon}^R f(x) dx - \text{divergent part as } R \rightarrow \infty, \epsilon \rightarrow 0 \right] \quad (\text{A.1})$$

A typical example is

$$\text{pf} \int_0^{r_0} \frac{dr}{r^n} = \begin{cases} \log r_0, & n = 1 \\ \frac{r_0^{1-n}}{1-n}, & n > 1 \end{cases} \quad (\text{A.2})$$

For small r_0 it then follows that

$$\text{pf} \int_0^{r_0} \frac{\dot{g}^1(r, \theta)}{r^n} dr = \begin{cases} (\log r_0) \dot{g}^1(0, \theta) + o(r_0), & n = 1 \\ \left(\frac{1}{1-n} r_0^{1-n} \right) \dot{g}^1(0, \theta) + o(r_0^{1-n}), & n > 1 \end{cases} \quad (\text{A.3})$$

where we have used that $\dot{g}^1(r, \theta)$ is bounded at $r=0$, see (4.3). Consistent with the definition (A.1), it is convenient to rewrite (4.18) in the form

$$\dot{I}_{>}(\theta, \theta_0) = \int_{-\pi}^{\pi} d\theta \left\{ \sum_{n=1}^{\infty} \left[\text{pf} \int_0^{\infty} \left(\frac{r_0}{r} \right)^{\frac{n+1}{2}} N_{n+1}(\theta, \theta_0) \dot{g}^1(r, \theta) dr - \text{pf} \int_0^{r_0} \left(\frac{r_0}{r} \right)^{\frac{n+1}{2}} N_{n+1}(\theta, \theta_0) \dot{g}^1(r, \theta) dr \right] \right\} \quad (\text{A.4})$$

By using (A.3), Eq.(A.4) can be rewritten as

$$\dot{I}_{>}(\theta, \theta_0) = f_2(\theta_0) r_0 \log r_0 + r_0 \dot{B}(\theta_0) + o(r_0) \quad (\text{A.5})$$

where

$\dot{f}_2(\theta_o)$ has been defined in (4.22) and

$$\dot{B}(\theta_o) = \int_{-\pi}^{\pi} d\theta [N_2(\theta, \theta_o) \text{ pf } \int_0^{\infty} \frac{\dot{q}^1(r, \theta)}{r} dr + \sum_{n=2}^{\infty} \frac{2}{n-1} N_{n+1}(\theta, \theta_o) \cdot \dot{q}^1(0, \theta)] \quad (\text{A.6})$$

Equation (A.5) shows that the order of $\dot{L}_>$ as $r \rightarrow 0$ is defined by terms $r_o \log r_o$ and r_o .

It is too complicated to compute all the terms in Eq.(A.6) by using the expansion given by (4.13). Another way of computing the relevant terms follows by considering Eq.(4.11) for the case $\dot{q}^1(r, \theta, t) \equiv 1$. From (4.11), (4.14), (4.17) and (A.5) it then follows that

$$\begin{aligned} \text{pf } \int_0^{\infty} r \dot{V} G dr &= r_o \left[\sum_{n=0}^{\infty} \frac{2}{n+3} M_{n+1}(\theta, \theta_o) + \sum_{\substack{n=-1 \\ n \neq 1}}^{\infty} \frac{2}{n-1} N_{n+1}(\theta, \theta_o) \right] \\ &\quad - N_2(\theta, \theta_o) r_o \log r_o \end{aligned} \quad (\text{A.7})$$

Next we define

$$P(\theta, \theta_o) = \frac{1}{r_o} \text{ pf } \int_0^{\infty} r \dot{V} G dr + N_2(\theta, \theta_o) \log r_o \quad (\text{A.8})$$

It can then be verified that

$$\dot{f}_3(\theta_o) = \int_{-\pi}^{\pi} P(\theta, \theta_o) \cdot \dot{q}^1(0, \theta) d\theta + \dot{C}_1 \begin{pmatrix} (\kappa+1)\cos\theta_o \\ (\kappa-3)\sin\theta_o \end{pmatrix} + \dot{C}_2 \begin{pmatrix} \sin\theta_o \\ -\cos\theta_o \end{pmatrix} \quad (\text{A.9})$$

The terms with the constants \dot{C}_1 and \dot{C}_2 come from the first integral of (A.6). The constant \dot{C}_2 (\dot{C}_1) vanishes for \dot{q}^1 having Mode I (II) symmetry.

The manipulations that are required to evaluate (A.8) by the use of (3.6) are lengthy and complicated. For the Mode-I case the result is given by Eq.(4.32).

Now that the third term in the expansion (4.23) is known explicitly, namely,

$$\dot{u}_2 = \dot{f}_2(\theta)r \log r \quad (A.10)$$

and it is known that \dot{u}_3 is of the form

$$\dot{u}_3 = \dot{f}_3(\theta)r, \quad (A.11)$$

an alternative way of computing $\dot{f}_3(\theta)$ is provided by returning to the substitution method outlined by Eqs.(4.1)-(4.6). By collecting terms of order r we find

$$\Delta_x^*[r\dot{f}_3(\theta)] = \Delta_x^*\dot{u}_2 + \nabla \cdot \sigma_1^i \quad (A.12)$$

A direct calculation shows that $r\Delta_x^*\dot{u}_2$ is a function of θ only. Hence the terms on the right hand side of (A.12) are r^{-1} times a function of θ . The standard Fredholm argument shows that for boundary conditions appropriate to Mode I, (A.12) does have a solution which is unique to within a term which would give rise to a uniform contribution to τ_{11} . The solution to (A.12) can now be determined by well established methods. The result is given by Eq.(4.32).

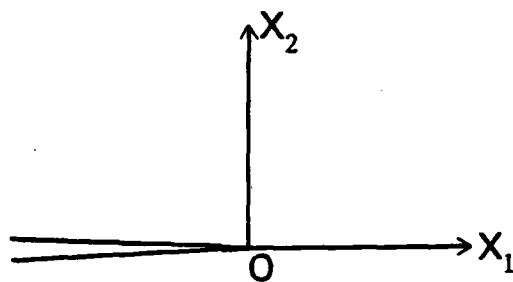


Fig. 1: Crack-tip geometry

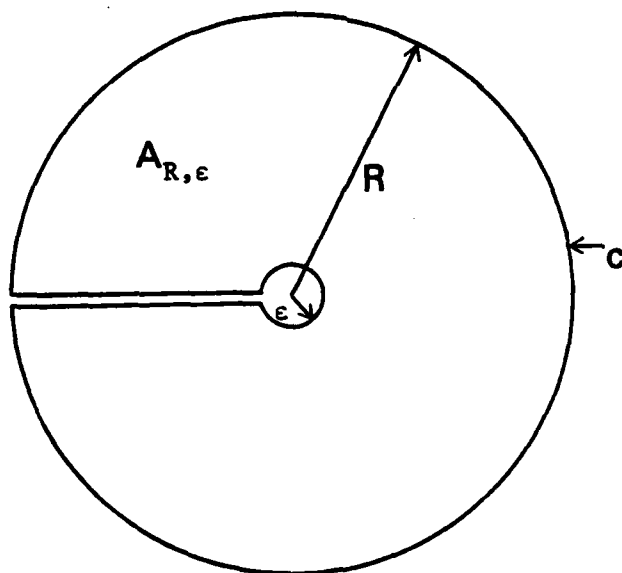


Fig. 2: Domain $A_{R,\epsilon}$ for use of integral identity

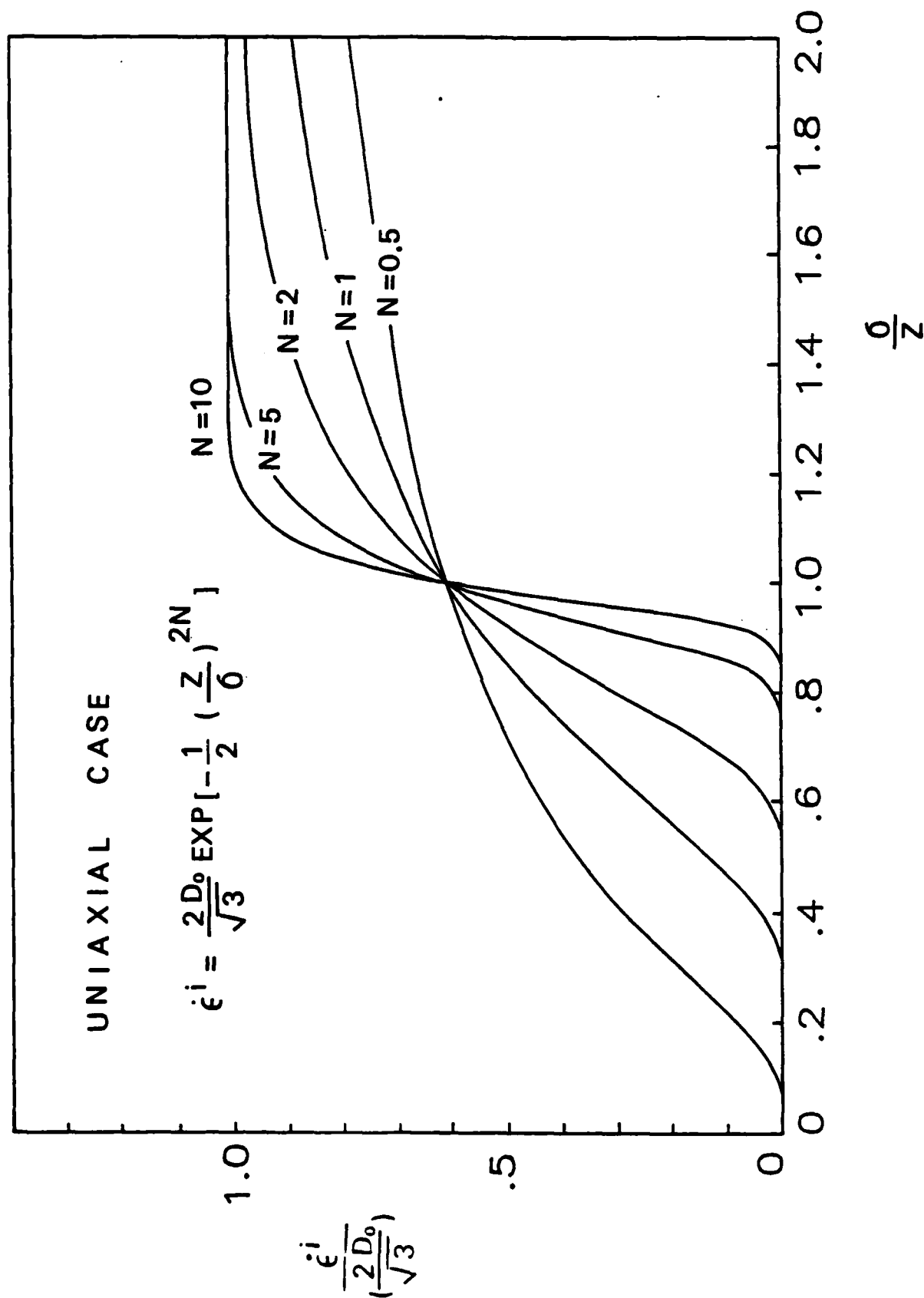


Fig. 3: Inelastic strain rates for uniaxial tension, σ , and various values of n .

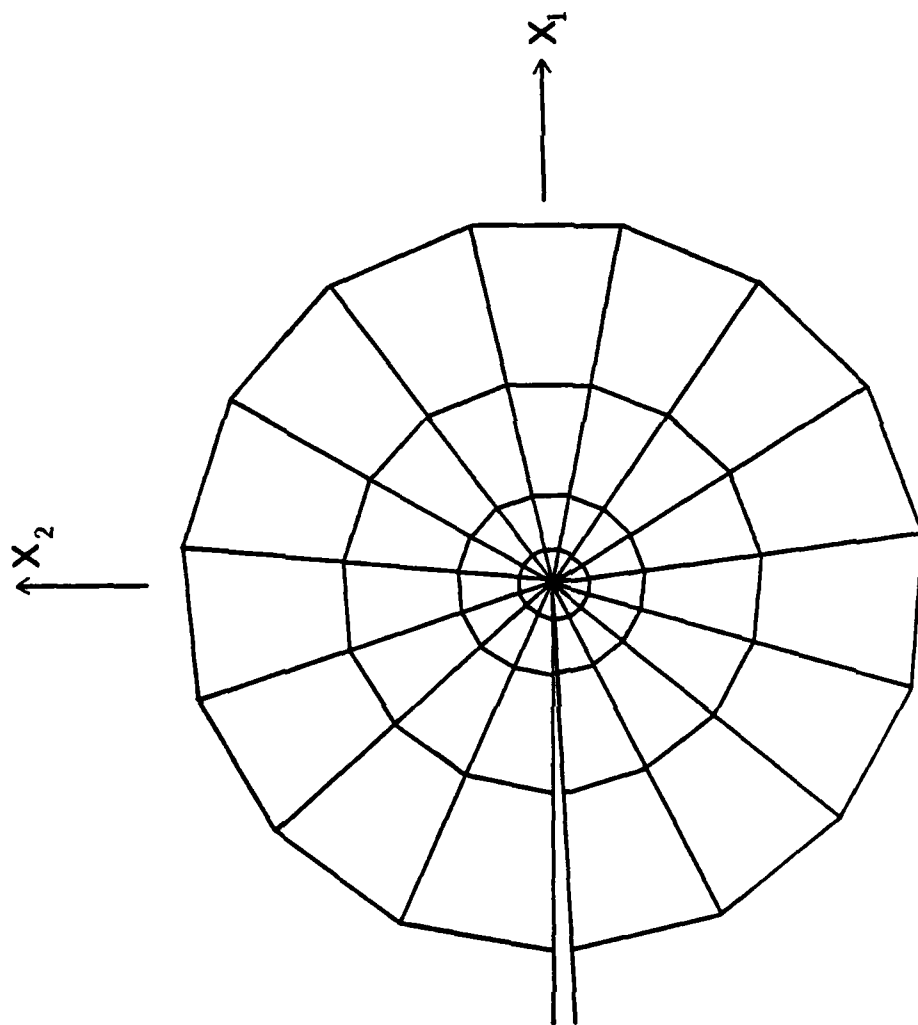


Fig. 4: Cell configuration for application of boundary integral equation method

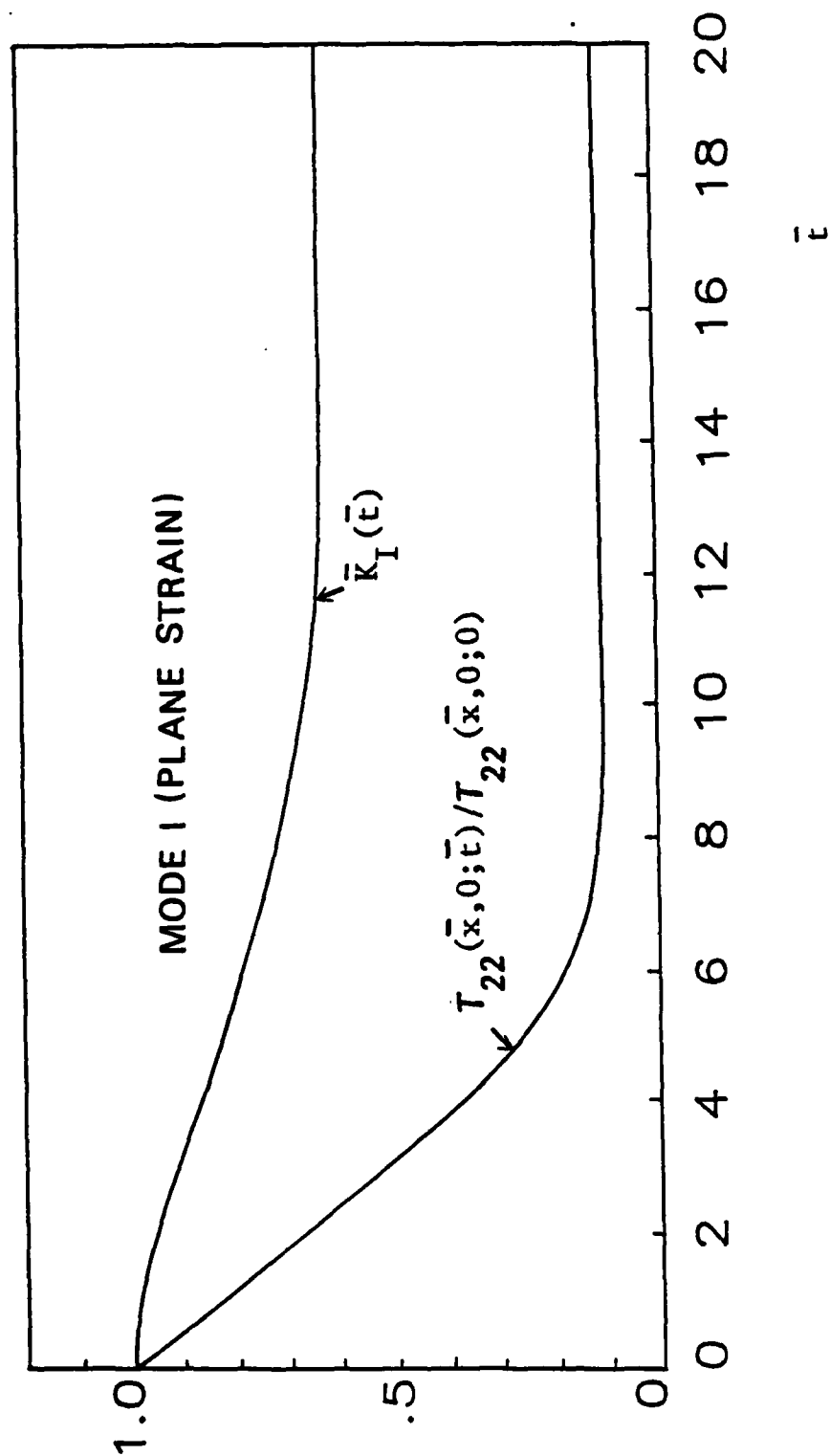


Fig. 5: Normalized opening stress at $\bar{x} = 0.0014$ and ratio $\bar{K}_I(\bar{t}) = K_I(\bar{t})/K_I(0)$, both as functions of dimensionless time, \bar{t} .

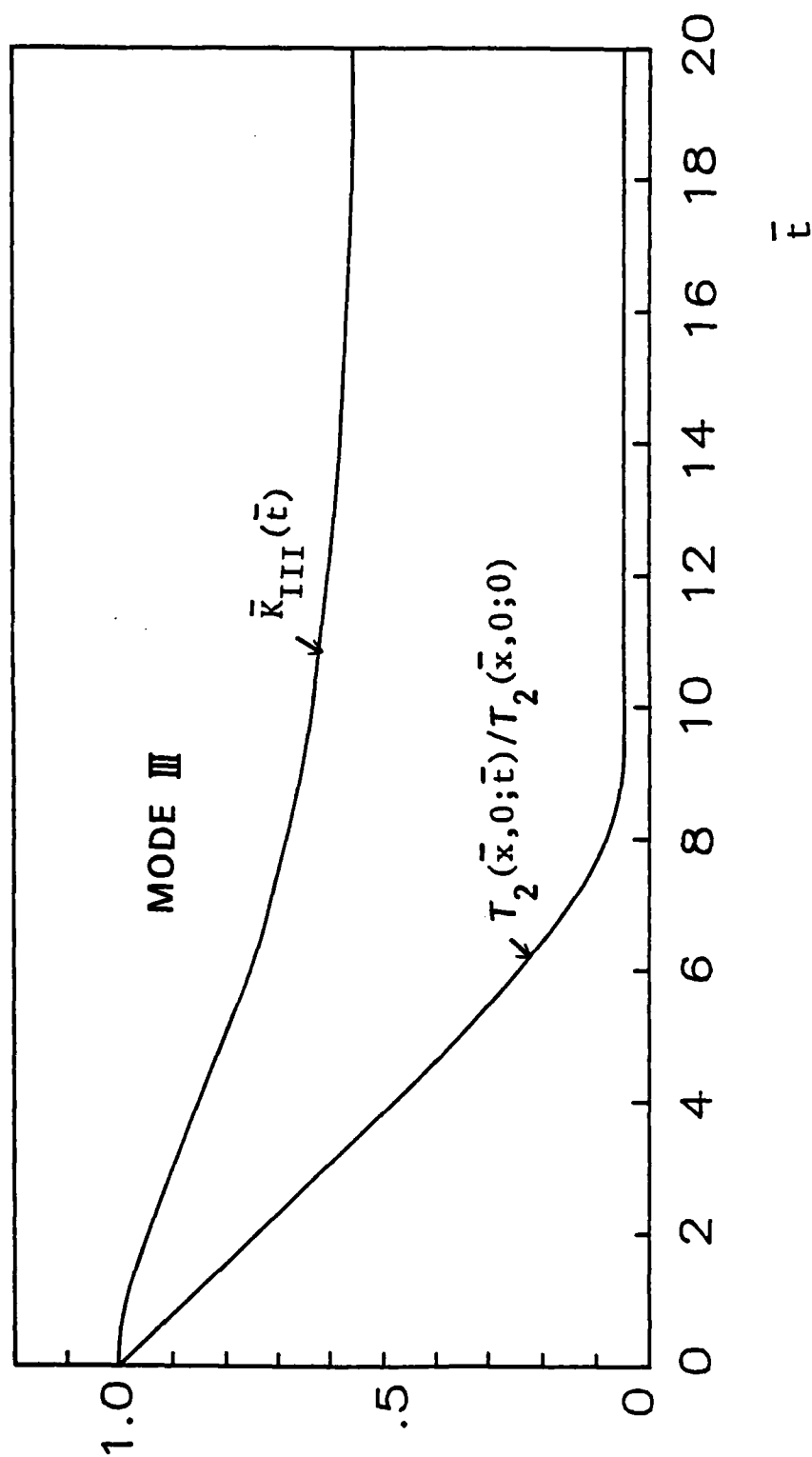


Fig. 6: Normalized anti-plane shear stress at $\bar{x} = 0.0047$ and ratio $\bar{K}_{III}(\bar{t}) = K_{III}(\bar{t})/K_{III}(0)$, both as functions of dimensionless time, \bar{t} .

	Mode I		Mode III	
$\frac{\tau_{22} D_o}{Z/\sqrt{3}}$	$\tau_{22}/(Z/\sqrt{3})$		$\tau_2/(Z/\sqrt{3})$	
	2 terms	BIEM	2 terms	BIEM
1	22.18	22.28	13.04	13.10
2	18.78	18.82	11.05	11.17
3	14.47	14.35	8.93	9.12
4	10.08	10.42	6.84	7.12

Table 1: Comparison of asymptotic representations with numerical results calculated by the BIEM.

Unclassified

SECURITY CLASSIFICATION OF THIS PAGE (When Data Entered)

REPORT DOCUMENTATION PAGE		READ INSTRUCTIONS BEFORE COMPLETING FORM
1. REPORT NUMBER NU-SML-TR-86-1	2. GOVT ACCESSION NO.	3. RECIPIENT'S CATALOG NUMBER
4. TITLE (and Subtitle) Crack-Tip Fields in a Viscoplastic Material		5. TYPE OF REPORT & PERIOD COVERED Interim
		6. PERFORMING ORG. REPORT NUMBER
7. AUTHOR(s) J. D. Achenbach, N. Nishimura and J. C. Sung		8. CONTRACT OR GRANT NUMBER(s) N00014-76-C-0063
9. PERFORMING ORGANIZATION NAME AND ADDRESS Northwestern University, Evanston, IL 60201		10. PROGRAM ELEMENT, PROJECT, TASK AREA & WORK UNIT NUMBERS
11. CONTROLLING OFFICE NAME AND ADDRESS Office of Naval Research Structural Mechanics Department Department of the Navy, Arlington, VA 22217		12. REPORT DATE April 1986
		13. NUMBER OF PAGES 37
14. MONITORING AGENCY NAME & ADDRESS (if different from Controlling Office)		15. SECURITY CLASS. (of this report) Unclassified
		15a. DECLASSIFICATION/DOWNGRADING SCHEDULE
16. DISTRIBUTION STATEMENT (of this Report) Approved for public release; distribution unlimited.		
17. DISTRIBUTION STATEMENT (of the abstract entered in Block 20, if different from Report)		
18. SUPPLEMENTARY NOTES		
19. KEY WORDS (Continue on reverse side if necessary and identify by block number) viscoplastic Mode I crack tip fields asymptotic analysis boundary integral equation method		
20. ABSTRACT (Continue on reverse side if necessary and identify by block number) An integral representation for the particle velocity in terms of a Green's function and certain linear combinations of the inelastic strain rates has been used in this paper, both for a numerical method to compute full field solutions and to develop unequivocal asymptotic expressions for the near-tip fields. Specific results have been obtained for a stationary crack in a solid whose constitutive behavior is represented by the Bodner-Partom model. It is shown that the leading term of the near-tip particle velocity is of order $r^{1/2}$, and the higher-order terms are of the forms $r \log r$ and r . Expressions have		

DD FORM 1 JAN 73 1473

EDITION OF 1 NOV 65 IS OBSOLETE

Unclassified

SECURITY CLASSIFICATION OF THIS PAGE (When Data Entered)

Unclassified

SECURITY CLASSIFICATION OF THIS PAGE(When Data Entered)

been derived for the angular variations and for the multiplying time-dependent intensity factors. The $r \log r$ term is absent for the Mode-III case. Two questions have been addressed in further detail: the dependence of the multiplying terms on time and the importance of the higher-order terms. The numerical results show a stress intensity factor which decays with time. At a small distance from the crack tip the numerically computed normalized opening stress $\tau_{22}(x_1, 0, t)/\tau_{22}(x_1, 0, 0)$ has been compared with a one-term asymptotic representation, i.e., with $K_I(t)/K_I(0)$. The two curves diverge at very small values of time. The inclusion of a second term in the asymptotic expression for the stress gives very acceptable agreement as time increases.

Unclassified

SECURITY CLASSIFICATION OF THIS PAGE(When Data Entered)

END

DTIC

6-86